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# Phase Equilibria in the Ln<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Ln=Dy and Ho) Systems at 1200 °C

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Phase equilibria in the systems,  $Dy_2O_3-V_2O_3-V_2O_5$  and  $Ho_2O_3-V_2O_5$ , were established at  $1200\,^{\circ}\text{C}$  by changing the oxygen partial pressure from 4.32 to -7.50 Pa in terms of  $\log Po_2$ . In both systems,  $Ln_2O_3$ ,  $LnVO_4$ ,  $LnVO_3$ ,  $V_nO_{2n-1}(n=2-7)$ ,  $VO_2$ , and  $Ln_8V_2O_{17}(4Ln_2O_3\cdot V_2O_5)$  are stable, and compounds with mole ratio  $Ln_2O_3/V_2O_5=5/1$  are not stable under the present experimental conditions. On the basis of the established phase diagrams, the standard Gibbs energies of reactions, (1)  $3Dy_2O_3+2Dy_2O_3+2Dy_2O_3+O_2=Dy_2O_1$ , (2)  $Dy_2O_3+1/2O_2=Dy_2O_3+1/2O_2=Dy_2O_3+1/2O_$ 

The phase equilibria in the Ln<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> systems1-8) at 1200 °C were established by changing the oxygen partial pressures from 4.32 (air) to -7.50 or -8.00 Pa in terms of  $\log P_{0_2}$ . These established phase diagrams showed different patterns one another because of the differences of compounds coexisting under the experimental conditions although systems with Gd<sub>2</sub>O<sub>3</sub>4) and Eu<sub>2</sub>O<sub>3</sub>8) showed a similar pattern. Besides, the standard Gibbs energies of reactions found in the established diagrams and crystallographic data of the compounds presented for the systems have been obtained. It has also been established that the relationship between the ionic radius and  $\Delta G^{\circ}$  of reaction, LnVO<sub>3</sub>+1/2 O<sub>2</sub>=LnVO<sub>4</sub>, is linear provided that the lanthanoid elements can be divided into two groups.

In the present study,  $Dy_2O_3$  and  $Ho_2O_3$  were chosen as  $Ln_2O_3$ . In the  $Dy_2O_3-V_2O_5$  and  $Ho_2O_3-V_2O_5$  systems, compounds with mole ratio  $Ln_2O_3/V_2O_5$  4/1 and 5/1 were stable<sup>9)</sup> in the air from 600 to 1500 °C in addition to the well-known  $LnVO_4$ . So new types of phase equilibria will be expected.

Only one report was available about  $Dy_2O_3-V_2O_3$  system, <sup>10)</sup> in which one compound  $DyVO_3$  with the congruent melting point at 2100 °C was found and it is nonstoichiometric toward  $V_2O_3$  side in the temperature range from about 1800 to 2000 °C. The  $Ho_2O_3-V_2O_3$  system has not been completely studied on account of the instability of  $V_2O_3$  in the air, but  $HoVO_3$  is well-known as a stable phase.

The crystallographic properties of DyVO<sub>3</sub>, HoVO<sub>3</sub>, DyVO<sub>4</sub>, and HoVO<sub>4</sub> were investigated by many researchers.<sup>11–14)</sup>

The objectives of the present study are: (1) preparation of the detailed phases diagrams of both systems at 1200 °C in order to determine the stable compounds under the present experimental conditions, (2) calculation of the standard Gibbs energies of reactions appeared in the established phase diagrams, and (3) examination of the fitness of present data on the linear relationship between the standard Gibbs energies of reactions and the ionic radius of the lanthanoid elements.

### **Experimental**

Analytical grades of Dy<sub>2</sub>O<sub>3</sub> (99.9%), Ho<sub>2</sub>O<sub>3</sub> (99.9%), and V<sub>2</sub>O<sub>5</sub>, which was made by heating NH<sub>4</sub>VO<sub>3</sub> of the guaranteed grade at 500 °C in the air for about 24 h, were used as the starting materials. Desired Dy<sub>2</sub>O<sub>3</sub>/V<sub>2</sub>O<sub>5</sub> and Ho<sub>2</sub>O<sub>3</sub>/V<sub>2</sub>O<sub>5</sub> mole ratios of samples were obtained by mixing appropriate quantities throughly in an agate motar under ethyl alcohol. The mixtures were treated by the procedures described in the previous paper.<sup>1)</sup> The apparatus and procedures for controlling the oxygen partial pressures and keeping a constant temperature, the method of thermogravimetry, the criterion for an equilibrium establishment, the method of measurement of the actual oxygen partial pressure, and the method of chemical analysis are the same as those reported in the previous papers.<sup>1,16–19)</sup>

## Results and Discussion

It was ascertained by the pre-Phase Equilibria. liminary studies that Dy<sub>2</sub>O<sub>3</sub> is stable under the present experimental ranges of the oxygen partial pressure. Seven samples with Dy<sub>2</sub>O<sub>3</sub>/V<sub>2</sub>O<sub>5</sub> mole ratios 85/15, 8/2, 7/3, 65/35, 1, 35/65, and 15/85 were prepared to be used in the thermogravimetric experiments. The thermogravimetric results for three samples with mole ratios 85/15, 7/3, and 35/65 are shown in Fig. 1 as representative. In Fig. 1 the ordinate is the oxygen partial pressure represented in log Po, in the Pa unit and the abscissa is the composition shown by  $W_{0}$  $W_{\rm T}$ , where  $W_{\rm O}$ , is the weight gain of the samples from the reference weight at  $\log P_{0_2} = -7.50$ , which is a point in the oxygen partial pressures where Dy<sub>2</sub>O<sub>3</sub>, DyVO<sub>3</sub>, and V<sub>2</sub>O<sub>3</sub> are stable, and W<sub>T</sub> is the total weight increase of samples which might get if V2O3 in the samples at the reference state changed to V<sub>2</sub>O<sub>5</sub> in the higher oxygen partial pressures. The  $Wo_2/W_T$ ratio was usually shown in the range from 0.995 to 1.00 in the air. Figure 1 shows the different patterns one another, and in the oxygen partial pressure range from  $\log P_{0} = -7.50$  to -4.85 (Fig. 1a) the weight change was not observed. The value of  $log Po_i = -4.85$ is the oxygen partial presure of the gas phase in equilibrium with the phase assemblages R+A<sub>2</sub>+

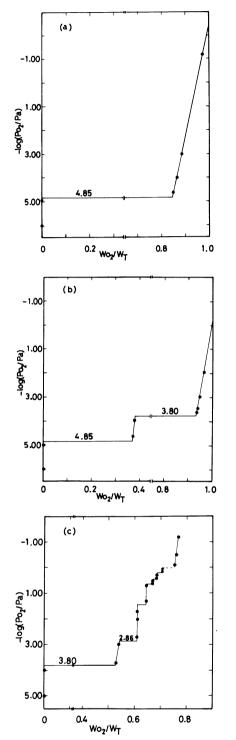


Fig. 1. The relationships between  $-\log(P_{\rm O_2}/{\rm Pa})$  and the compositions,  $W_{\rm O_2}/W_{\rm T}$ , of the samples. (a)  ${\rm Dy_2O_3/V_2O_5}{=}85/15$ , (b)  ${\rm Dy_2O_3/V_2O_5}{=}7/3$ , (c)  ${\rm Dy_2O_3/V_2O_5}{=}35/65$ .

C which symboles will be shown in Table 2. In the range higher than  $\log Po_i=-4.85$ , the weight changes linearly with the change in oxygen partial pressures. Figure 1b shows two oxygen partial pressures, -4.85 and -3.80 in  $\log Po_i$ , in equilibrium. The latter corresponds to that of Reaction (2) in Table 4, and Fig. 1c have six oxygen partial pressures in equilibrium

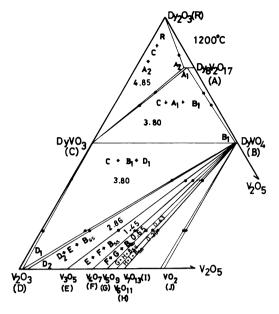


Fig. 2. Phase equilibria in the  $\mathrm{Dy_2O_3-V_2O_3-V_2O_5}$  system at 1200 °C. Numerical values in the three solid phases regions are the oxygen partial pressures in equilibrium in  $-\log P_{\mathrm{O_2}}$ . Symbols are the same as those in Table 2.

in which five values correspond to those of the reactions in the V-O system.<sup>1)</sup>

In Table 1 the results of identification of phases are shown. In the first column are shown the compositions of the starting materials in mole%, in the second the experimental conditions of the oxygen partial pressure in terms of  $\log Po_2$  in Pa, in the third the experimental durations in hours, and in the last the phases that were found in the respective quenched samples using X-ray powder diffractometer with Cu  $K\alpha$  radiation.

Based upon the above thermogravimetric results and the results of identification of phases, a phase diagram of the system can be constructed and is shown in Fig. 2. The following phases are stable;  $V_nO_{2n-1}(n=2-7)$ ,  $VO_2$ ,  $Dy_2O_3$ ,  $DyVO_4$ ,  $DyVO_3$ , and  $Dy_8V_2O_{17}(4Dy_2O_3 \cdot V_2O_5)$ . The compound  $5Dy_2O_3 \cdot V_2O_5$  reported by Brusset *et al.*<sup>9)</sup> as the stable phase was not found.

The stability of  $\text{Ho}_2\text{O}_3$  under the present experimental conditions was confirmed by preliminary experiments. Seven samples with  $\text{Ho}_2\text{O}_3/\text{V}_2\text{O}_5$  mole ratios 85/15, 8/2, 7/3, 6/4, 1, 35/65, and 15/85 have also been used in the thermogravimetric experiments. The value of  $\log P_{\text{O}_2}$ =-7.50 was selected as the reference oxygen partial pressure by the similar reason as described above. In Fig. 3 the relationships between the oxygen partial pressure and the composition of samples are shown as those in Fig. 1 with the representative samples having mole ratios 85/15, 6/4, and 15/85. Figure 3 shows similar patterns to Fig. 1.

Quenched samples were used for the identification of phases and the phases were identified by X-ray powder diffractometer with Cu  $K\alpha$  radiation. The results are shown in Table 1 together with those of the Dy<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> system. Figure 4 was depicted by using

above experimental results as those in Fig. 2. Figures. 2 and 4 give similar patterns each other. In addition to the seven oxides in the  $V_2O_3$ – $V_2O_5$  system,  $Ho_2O_3$ ,  $HoVO_4$ ,  $HoVO_3$ , and  $Ho_8V_2O_{17}(4Ho_2O_3\cdot V_2O_5)$  are stable. These phase diagrams are very simple having only one compound between  $Ln_2O_3$  and  $LnVO_4$ . This type of the phase diagram was found in the systems of Eu, Gd, and Er. It was very interesting that

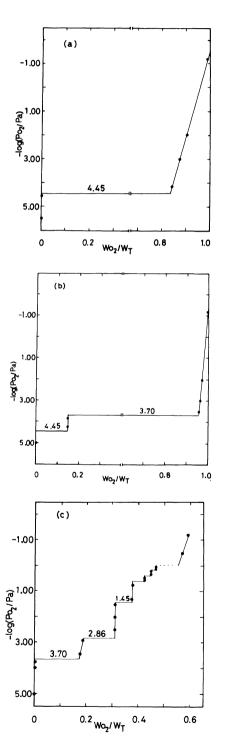


Fig. 3. The relationships between  $-\log(P_{\rm O_2}/{\rm Pa})$  and the compositions,  $W_{\rm O_2}/W_{\rm T}$  of samples. (a)  ${\rm Ho_2O_3/V_2O_5}{=}85/15$ , (b)  ${\rm Ho_2O_3/V_2O_5}{=}6/4$ , (c)  ${\rm Ho_2O_3/V_2O_5}{=}15/85$ .

TABLE 1. IDENTIFICATION OF PHASES

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Starting materials		$-\log(Po_2)$	Time	Di
85				h	Phases
85	$Dy_2O_3$	$V_2O_5$			
5.00	85		7.50	8	$Dy_2O_3 + DyVO_3$
4.50				27	
65   35   7.50   8   Dy <sub>2</sub> O <sub>3</sub> + DyVO <sub>3</sub>     5.00   27   Dy <sub>2</sub> O <sub>3</sub> + DyVO <sub>3</sub>     4.50   22   DyVO <sub>3</sub> + Dy <sub>8</sub> V <sub>2</sub> O <sub>1</sub>     2.50   27   DyVO <sub>4</sub> + Dy <sub>8</sub> V <sub>2</sub> O <sub>1</sub>     -4.32   63   DyVO <sub>4</sub> + Dy <sub>8</sub> V <sub>2</sub> O <sub>2</sub>     -4.32   63   DyVO <sub>4</sub> + Dy <sub>8</sub> V <sub>2</sub> O <sub>2</sub>     -4.32   63   DyVO <sub>4</sub> + V <sub>2</sub> O <sub>3</sub>     3.30   28   DyVO <sub>4</sub> + V <sub>2</sub> O <sub>3</sub>     2.00   27   DyVO <sub>4</sub> + V <sub>3</sub> O <sub>5</sub>     1.00   28   DyVO <sub>4</sub> + V <sub>3</sub> O <sub>5</sub>     0.35   41   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>6</sub>     0.35   41   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>1</sub>     0.10   56   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>3</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub>     -0.55   39   DyVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -0.55   48   HoVO <sub>4</sub> + V <sub>5</sub> O <sub>5</sub>     -					
5.00			-4.32	63	${\rm Dy_2O_3} \! + \! {\rm Dy_8V_2O_{17}}$
5.00	65	35	7.50	8	$D_{V_2}O_3 + D_VVO_3$
2.50			5.00	27	
-4.32			4.50	22	$\mathrm{DyVO_3} + \mathrm{Dy_8V_2O_{17}}$
35 65 7.50 8 DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> 3.30 28 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 2.00 27 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>5</sub> 1.00 28 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>7</sub> 0.55 39 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>1</sub> 0.10 56 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>1</sub> 0.0.55 39 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.33 22 DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> 0.20 27 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.33 28 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.05 39 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>9</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>9</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>1</sub> 0.10 56 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>1</sub> 0.10 60 24 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>3</sub> V <sub>2</sub> O <sub>1</sub> 0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.30 47 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.30 47 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.30 47 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.30 47 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 26 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 0.00 0.00 48 Ho <sub>2</sub> O <sub>4</sub> +			2.50	27	$\mathrm{DyVO_4} + \mathrm{Dy_8V_2O_{17}}$
4.50   22   DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     3.30   28   DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     2.00   27   DyVO <sub>4</sub> +V <sub>3</sub> O <sub>5</sub>     1.00   28   DyVO <sub>4</sub> +V <sub>4</sub> O <sub>7</sub>     0.55   39   DyVO <sub>4</sub> +V <sub>5</sub> O <sub>9</sub>     0.35   41   DyVO <sub>4</sub> +V <sub>6</sub> O <sub>11</sub>     0.10   56   DyVO <sub>4</sub> +V <sub>7</sub> O <sub>13</sub>     -0.55   39   DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     4.50   22   DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     4.50   22   DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     3.30   28   DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     2.00   27   DyVO <sub>4</sub> +V <sub>3</sub> O <sub>5</sub>     1.00   28   DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     2.00   27   DyVO <sub>4</sub> +V <sub>5</sub> O <sub>9</sub>     0.35   41   DyVO <sub>4</sub> +V <sub>5</sub> O <sub>11</sub>     0.10   56   DyVO <sub>4</sub> +V <sub>7</sub> O <sub>13</sub>     -0.55   39   DyVO <sub>4</sub> +V <sub>0</sub> O <sub>11</sub>     0.10   56   DyVO <sub>4</sub> +V <sub>0</sub> O <sub>11</sub>     0.10   48   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     4.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     4.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     3.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     3.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     4.32   63   Ho <sub>2</sub> O <sub>4</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     3.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     4.32   63   Ho <sub>2</sub> O <sub>4</sub> +V <sub>4</sub> O <sub>3</sub>     4.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     3.00   24   Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>4</sub> O <sub>2</sub> O <sub>17</sub>     0.10   48   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     4.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     4.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   48   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   48   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   48   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   48   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>     1.00   24   Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub>			-4.32	63	$\mathrm{DyVO_4} + \mathrm{Dy_8V_2O_{17}}$
3.30	35	65	7.50	8	
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15 85 7.50 8 DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> 4.50 22 DyVO <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> 3.30 28 DyVO <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> 2.00 27 DyVO <sub>4</sub> +V <sub>3</sub> O <sub>5</sub> 1.00 28 DyVO <sub>4</sub> +V <sub>4</sub> O <sub>7</sub> 0.55 39 DyVO <sub>4</sub> +V <sub>5</sub> O <sub>9</sub> 0.35 41 DyVO <sub>4</sub> +V <sub>6</sub> O <sub>11</sub> 0.10 56 DyVO <sub>4</sub> +V <sub>0</sub> O <sub>13</sub> -0.55 39 DyVO <sub>4</sub> +V <sub>0</sub> O <sub>13</sub> -0.55 40 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>2</sub> V <sub>0</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>2</sub> V <sub>0</sub> O <sub>17</sub> -0.4.32 63 Ho <sub>2</sub> O <sub>3</sub> +Ho <sub>2</sub> V <sub>0</sub> O <sub>17</sub> -0.55 60 Ho <sub>2</sub> O <sub>4</sub> Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>13</sub> -0.50 32 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.50 46 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.50 47 Ho <sub>2</sub> O <sub>3</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.55 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.56 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub> O <sub>3</sub> -0.57 48 Ho <sub>2</sub> O <sub>4</sub> +V <sub>2</sub>					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.5	0.5			
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Ho <sub>2</sub> O <sub>3</sub>	$V_2O_5$			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	85	15	6.00	24	Ho <sub>2</sub> O <sub>3</sub> + HoVO <sub>3</sub>
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			4.00	24	${\rm Ho_2O_3} + {\rm Ho_8V_2O_{17}}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			-4.32	63	$\mathrm{Ho_{2}O_{3}}\!+\!\mathrm{Ho_{8}V_{2}O_{17}}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	70	30	6.00	24	$Ho_2O_3 + HoVO_3$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			3.90	24	$\mathrm{Ho_{2}O_{3}}\!+\!\mathrm{Ho_{8}V_{2}O_{17}}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				24	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			-4.32	63	$HoVO_4 + Ho_8V_2O_{17}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	65	6.00	24	$HoVO_3 + V_2O_3$
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	15	85	6.00	24	$HoVO_3 + V_2O_3$
$\begin{array}{ccccc} 2.00 & 26 & \text{HoVO}_4 + \text{V}_3\text{O}_5 \\ 1.00 & 48 & \text{HoVO}_4 + \text{V}_4\text{O}_7 \\ 0.55 & 48 & \text{HoVO}_4 + \text{V}_5\text{O}_9 \\ 0.30 & 47 & \text{HoVO}_4 + \text{V}_6\text{O}_{11} \\ 0.10 & 48 & \text{HoVO}_4 + \text{V}_7\text{O}_{13} \end{array}$			4.00	24	$HoVO_3 + V_2O_3$
$\begin{array}{cccc} 1.00 & 48 & \text{HoVO}_4 + \text{V}_4^{\text{O}_7} \\ 0.55 & 48 & \text{HoVO}_4 + \text{V}_5^{\text{O}_9} \\ 0.30 & 47 & \text{HoVO}_4 + \text{V}_6^{\text{O}_{11}} \\ 0.10 & 48 & \text{HoVO}_4 + \text{V}_7^{\text{O}_{13}} \end{array}$					
$egin{array}{lll} 0.55 & 48 &  ext{HoVO}_4 +  ext{V}_5  ext{O}_9 \ 0.30 & 47 &  ext{HoVO}_4 +  ext{V}_6  ext{O}_{11} \ 0.10 & 48 &  ext{HoVO}_4 +  ext{V}_7  ext{O}_{13} \ \end{array}$					$H_0VO_4 + V_3O_5$
$egin{array}{lll} 0.30 & 47 &  ext{HoVO}_4 +  ext{V}_6  ext{O}_{11} \ 0.10 & 48 &  ext{HoVO}_4 +  ext{V}_7  ext{O}_{13} \ \end{array}$					
$0.10   48   \text{HoVO}_4 + \text{V}_7 \text{O}_{13}$					
			0.10	48	$HoVO_4 + V_7O_{13}$
			-0.50	32	

these elements are located in the middle of the lanthanoid.

DyVO<sub>4</sub>, HoVO<sub>4</sub>, Dy<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, and Ho<sub>8</sub>V<sub>2</sub>O<sub>17</sub> have nonstoichiometric compositions, and the relationships between the oxygen partial pressure and the compositions were obtained as follows:  $N_{\rm O}/N_{\rm B}$ =4.23×  $10^{-3}\log P_{\rm O_2}$ -1.38× $10^{-4}$  for DyVO<sub>4</sub>,  $N_{\rm O}/N_{\rm L}$ =8.80×  $10^{-3}\log P_{\rm O_2}$ +6.37× $10^{-3}$  for HoVO<sub>4</sub>,  $N_{\rm O}/N_{\rm A}$ =0.045 log  $P_{\rm O_2}$ -0.098 for Dy<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, and  $N_{\rm O}/N_{\rm K}$ =0.079 log  $P_{\rm O_2}$ -0.023 for Ho<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, where N<sub>O</sub> is the mole fraction

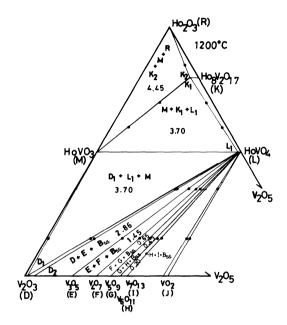


Fig. 4. Phase equilibria in the  $\text{Ho}_2\text{O}_3\text{-}\text{V}_2\text{O}_3\text{-}\text{V}_2\text{O}_5$  system at 1200 °C. Numerical values in the three solid phases regions are the oxygen partial pressures in equilibrium in  $-\log P_{\text{O}_2}$ . Symbols are the same as those in Table 2.

of oxygen atom in the compounds and  $N_A$ ,  $N_B$ ,  $N_K$ , and  $N_L$  are the mole fractions of the Dy<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, DyVO<sub>4</sub>, Ho<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, and HoVO<sub>4</sub> components in the compounds, respectively.

Table 2 lists the compositions of the compounds at various oxygen partial pressures, stability ranges of the compounds in terms of  $\log Po_2$ , the symbols of the compounds, and the activities of the components described above. The activities of the components in the solid solutions were calculated by means of the Gibbs-Duhem equation with the data of thermogravimetry, for example  $N_0/N_A$  vs.  $\log Po_2$  described above. A detailed method of the calculation has been discussed in the previous paper. 18)

Lattice constants of the compounds DyVO<sub>3</sub>, DyVO<sub>4</sub>, Dy<sub>8</sub>V<sub>2</sub>O<sub>17</sub>, HoVO<sub>3</sub>, HoVO<sub>4</sub>, and Ho<sub>8</sub>V<sub>2</sub>O<sub>17</sub> are tabulated in Table 3. Present values are in good agreement

Table 2. Compositions, symbols, stability ranges in the oxygen partial pressures, and activities of component in the solid solutions

Component	Composition	Symbol	$-\log(P_{\rm O_2}/{\rm Pa})$	$-\log a_{\rm i}$
$\overline{\mathrm{Dy_8V_2O_{17}}}$	Dy <sub>8</sub> V <sub>2</sub> O <sub>17.0</sub>	A	$-2.1^{a}$ $-4.32$	0.55
	$Dy_8V_2O_{16.73}$	$\mathbf{A_1}$	3.80	0.15
	$\mathrm{Dy_8V_2O_{16.69}}$	$\mathbf{A_2}$	4.85	0
DyVO <sub>4</sub>	DyVO <sub>4.00</sub>	В	$0.0^{a}$ — $-4.32$	0.016
	$\mathrm{DyVO_{3.98}}$	$\mathbf{B_1}$	3.80	0
$Ho_8V_2O_{17}$	Ho <sub>8</sub> V <sub>2</sub> O <sub>17.0</sub>	K	$-0.3^{a}$ $-4.32$	0.45
	$\mathrm{Ho_{8}V_{2}O_{16.7}}$	$K_1$	3.70	0.13
	$\mathrm{Ho_8V_2O_{16\cdot6}}$	$\mathbf{K_2}$	4.45	0
HoVO <sub>4</sub>	HoVO <sub>4.00</sub>	L	0.7a) — - 4.32	0.020
	HoVO <sub>3.97</sub>	$\mathbf{L_1}$	3.70	0

a) These values were obtained by extrapolating the thermogravimetric results.

TABLE 3. CELL DIMENSIONS OF COMPOUNDS

Sample	$-\log(P_{O_2}/Pa)$	Å	<u>b</u>	- c A	<u>β</u> .	$\frac{V}{{ m \AA}^3}$	Ref
DyVO <sub>3</sub>	7.50	$5.311 \pm 0.003$	$5.618 \pm 0.003$	$7.602 \pm 0.004$		$226.8 \pm 0.2$	
	5.00	$5.305 \pm 0.002$	$5.613 \pm 0.002$	$7.603 \pm 0.002$		$226.4 \pm 0.2$	
		5.299	5.594	7.593		225.1	11
		5.302	5.602	7.601			12
DyVO <sub>4</sub>	-4.32	$7.157 \pm 0.002$		6.317±0.002		$323.6 \pm 0.2$	
	3.50	$7.157 \pm 0.002$		$6.315 \pm 0.002$		$323.5 \pm 0.2$	
		7.1434		6.313			13
$Dy_8V_2O_{17}$	-4.32	$10.69 \pm 0.05$	$8.81 \pm 0.14$	15.75 ±0.12	$99.1 \pm 0.5$	$1460 \pm 20$	
	4.50	$10.71 \pm 0.08$	$8.65 \pm 0.08$	$15.48 \pm 0.28$	$98.8 \pm 0.5$	$1420\pm30$	
HoVO <sub>3</sub>	4.00	$5.283 \pm 0.002$	$5.609 \pm 0.002$	$7.580 \pm 0.002$		$224.6 \pm 0.2$	
	6.00	$5.277 \pm 0.002$	$5.597 \pm 0.002$	$7.579 \pm 0.002$		$223.8 \pm 0.2$	
		5.276	5.592	7.576		223.5	11
HoVO <sub>4</sub>	-4.32	$7.129 \pm 0.002$		$6.293 \pm 0.002$	N 118 T	$319.8 \pm 0.2$	
	3.50	$7.129 \pm 0.002$		$6.300 \pm 0.004$		$320.2 \pm 0.3$	
		7.1214		6.2926			14
Ho <sub>8</sub> V <sub>2</sub> O <sub>17</sub>	-4.32	$10.69 \pm 0.10$	$8.43 \pm 0.05$	$15.22 \pm 0.36$	98.4±0.7	$1360 \pm 35$	
	4.00	$10.65 \pm 0.08$	$8.61 \pm 0.07$	$15.49 \pm 0.28$	$99.0 \pm 0.5$	$1400\pm30$	

TABLE 4. THE STANDARD GIBBS ENERGIES OF REACTIONS

Reaction	$-\log(P_{O_2}/\mathrm{Pa})$	$\frac{-\Delta G^{\circ}}{\mathrm{kJ}}$
(1) $3 Dy_2O_3 + 2 DyVO_3 + O_2$ = $Dy_8V_2O_{17}$	$4.85 \pm 0.05$	278±1
(2) $DyVO_3 + 1/2 O_2 = DyVO_4$	$3.80 \pm 0.03$	$123.8\!\pm\!0.5$
(3) $3 \operatorname{Ho_2O_3} + 2 \operatorname{HoVO_3} + O_2$ = $\operatorname{Ho_8V_2O_{17}}$	$4.45 \pm 0.07$	277±2
(4) $HoVO_3 + 1/2 O_2 = HoVO_4$	$3.70{\pm}0.03$	$122.4 \pm 0.5$

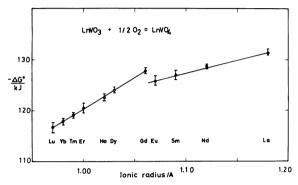


Fig. 5. The relationship between the ionic radius of lanthanoid elements with eight coordination and the  $\Delta G^{\circ}$  values of reaction,  $LnVO_3 + 1/2 O_2 = LnVO_4$ .

with those quoted in the Table. There are no considerable differences in values of the samples which were prepared under the different conditions of oxygen partial pressures. Lattice constants of Dy<sub>8</sub>V<sub>2</sub>O<sub>17</sub> and Ho<sub>8</sub>V<sub>2</sub>O<sub>17</sub> were determined with the data of 4 Tm<sub>2</sub>O<sub>3</sub>. V<sub>2</sub>O<sub>5</sub>.<sup>20)</sup> Experimental errors are still large compared with the data of other compounds.

Calculation of the Standard Gibbs Energies of Reactions. On the basis of the present phase equilibria, the standard Gibbs energies of the reactions appeared in the systems, except for the partial system of V<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub>, can be calculated by an equation,  $\Delta G^{\circ} = -RT \ln K$ , where R is the gas constant, T, the absolute temperature, and K, the equilibrium constant of each reaction. Chemical reactions appeared in the phase diagrams, the oxygen partial pressures in equilibrium for each reaction, and  $\Delta G^{\circ}$  values obtained are shown in Table 4. Activities of each component in solid solutions, which are necessary for the calculation, are given in Table 2.

The Relationship between  $\Delta G^{\circ}$  and Ionic Radius. In the series of Ln<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> system, the common reaction, LnVO<sub>3</sub>+1/2 O<sub>2</sub>=LnVO<sub>4</sub>, appeares in all the systems. It is very interesting to correlate the  $\Delta G^{\circ}$ values of reactions with some properties of lanthanoid elements. In a previous report,7) we have graphically presented the linear relationship between  $\Delta G^{\circ}$  values and the ionic radius of lanthanoid elements with eight coordination, provided that the lanthanoid series was subdivided into two groups. The present program is to ascertain whether or not the data obtained in the present systems fit well to the previous linear relation. The values of the present systems are plotted in Fig. 5 with open circles. These circles are well fit on the line which has been drawn using the data of previous results of another systems.

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